

efficiency and quality of carried out works, provided necessary accuracy, interchangeability and reliability. Research of «new technology», in conjunction with the integrated systems and laser means of measurement allows to raise considerably competitiveness of the integrated adaptive through system of stamps manufacture.

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Distributed control of ore beneficiation interrelated processes under parametric uncertainty



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Abstract

A method of distributed control forming of ore beneficiation interrelated processes under parametric uncertainty using robust control techniques is proposed.

Key words: DISTRIBUTED AND ROBUST CONTROL, ORE DRESSING

Problems of technological processes control synthesis of iron ore raw material beneficiation as the complex objects with a large number of parameters and disturbing influences are discussed in a significant number of works.

In particular, in papers [1-4] there noted that under parametric uncertainty and considerable spatial extent of ore beneficiation technological lines, the control effectiveness is greatly reduced.

It should be noted that a significant impact on the results of the beneficiation process have the characteristics of individual mineralogical and technological ore varieties and their relationship in the factory process flows [5-9].

The changes in these characteristics, along with the wear of technological units mechanisms, leads to the drift of control objects parameters. Under these conditions, during the control formation of ore-dressing plant technological lines it is advisable to use the methods of distributed and robust control [1-2].

Thus, ore beneficiation technological line as the control object must be represented as a system with concentrated inputs and output distributed in time and space. In this case, the concentrated system inputs are the effects on the individual technological units, the most common of which is the regulation of the ore-water ratio.

The distributed output is the distribution function of the mineral content by ore material size classes in technological units and conveyor lines, which are linking them.

In accordance with the formulation proposed in [1], the problem of distributed control of iron ore beneficiation technological line is the following. It is necessary to form a specific sequence of control actions $\bar{Q}(k)$, which set the ratio of ore and water for local technological units. Thus, it is necessary to provide a minimum deviation of the iron content in size classes $\beta(x, k)$ from a given value $\beta^*(x, \infty)$

$$\varepsilon(x, k) = \beta^*(x, \infty) - \beta(x, k), \quad (1)$$

which will have a minimum value $\varepsilon_{\min}(x, \infty)$ under the quadratic norm

$$\varepsilon_{\min}(x, \infty) = \min \left\| \beta^*(x, \infty) - \beta(x, k) \right\| \quad (2)$$

At the initial stage, it is necessary to obtain the problem solution of approximation in the block of spatial control synthesis. During the beneficiation technological line control, this problem, will take the following form according to [1]

$$\min \left\| \beta^*(x, \infty) - \sum_{i=1}^n \beta_i(x_i, \infty) HR_i(x, \infty) \right\| \quad (3)$$

where $\{HR_i(x, \infty)\}_i$ – are the steady values of given transfer characteristics of beneficiation units; $\{\beta_i^*(x_i, \infty)\}_i$ – are the approximation parameters. The resulting vector of optimal approximation $\{\tilde{\beta}_i^*(x_i, \infty)\}_i$ is supplied to the input of the temporal synthesis, which consists of a single-channel control circuits with concentrated parameters. A typical circuit comprises a control object with zero-order predictor and controller with concentrated parameters (Fig. 1).

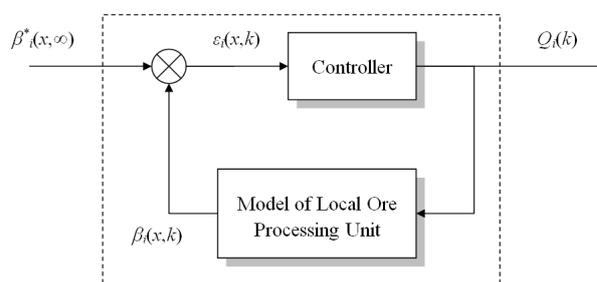


Figure 1. Single-circuit control system of ore beneficiation line local technological unit

In control problems solving the beneficiation technological line units, in the most general case, excluding net delay are present in the form of differential equations of the first and second orders [10]

$$\mu \frac{d^2 \beta(t)}{dt^2} + \theta \frac{d\beta(t)}{dt} + \kappa \beta(t) = Q(t). \quad (2)$$

The nonstationarity characteristics of iron ore raw materials and technological units mechanisms wear in the process of their work should be taken into account in the model. For this, let's assume that the values of its parameters μ, θ, κ can deviate from the nominal values $\bar{\mu}, \bar{\theta}, \bar{\kappa}$ on certain values $-1 \leq \delta_\mu, \delta_\theta, \delta_\kappa \leq 1$. Considering the parameters uncertainty μ, θ, κ it is advisable to present them in the form of two blocks obtained using linear fractional transformation and connecting to the top of the respective blocks $\delta_\mu, \delta_\theta, \delta_\kappa$ [2, 11]. As a result, the output signals of the parameters blocks

with model uncertainty of local technological units of iron ore beneficiation line can be written as [2]

$$\begin{bmatrix} y_\mu \\ x'' \end{bmatrix} = \begin{bmatrix} -p_\mu & 1/\sqrt{\mu} \\ -p_\mu & 1/\sqrt{\mu} \end{bmatrix} \begin{bmatrix} Q_\mu \\ Q - v_\theta - v_\kappa \end{bmatrix}; \begin{bmatrix} y_\theta \\ v_\theta \end{bmatrix} = \begin{bmatrix} 0 & \bar{\theta} \\ p_\theta & \bar{\theta} \end{bmatrix} \begin{bmatrix} Q_\theta \\ x' \end{bmatrix}; \begin{bmatrix} y_\kappa \\ v_\kappa \end{bmatrix} = \begin{bmatrix} 0 & \bar{\kappa} \\ p_\kappa & \bar{\kappa} \end{bmatrix} \begin{bmatrix} Q_\kappa \\ x \end{bmatrix}, \quad (3)$$

In general, the model of local technological units of beneficiation line with uncertain parameters can be written as [2, 11]

$$\beta = F_Q(G_{SM}, \Delta_{(\mu\theta\kappa)})Q, \quad (4)$$

where $\Delta_{(\mu\theta\kappa)}$ – is the diagonal matrix of uncertainties ($\delta_\mu, \delta_\theta, \delta_\kappa$).

To minimize the error energy for the most unfavorable value of the input disturbance it is advisable to use H_∞ -norm as an optimality criterion. The calculation of H_∞ -norm is performed on the basis of the matrix in the state space [11].

$$H = \begin{bmatrix} A & BB^T \\ -CC^T & -A^T \end{bmatrix}. \quad (5)$$

$$S = (I + GK)^{-1}; R = K(I + GK)^{-1}; T = GK(I + GK)^{-1}. \quad (7)$$

Choosing of weighting functions was carried out in accordance with the recommendations outlined in [13].

$$\overline{\sigma}(S(j\omega)) \leq \gamma \underline{\sigma}(W_1^{-1}(j\omega)); \overline{\sigma}(R(j\omega)) \leq \gamma \underline{\sigma}(W_2^{-1}(j\omega)); \overline{\sigma}(T(j\omega)) \leq \gamma \underline{\sigma}(W_3^{-1}(j\omega)), \quad (8)$$

where γ – is the positive number.

Thus, as shown in [1], the parametric synthesis

where $Q_\mu = \delta_\mu y_\mu, Q_\theta = \delta_\theta y_\theta, Q_\kappa = \delta_\kappa y_\kappa$.

Problem solution of formation of local concentrating units control, was carried out by the synthesis of the controller transfer function, which minimizes the function [11, 12]

$$T_{y1u1} = [W_1 S \quad W_2 R \quad W_3 T]^T, \quad (6)$$

where $W_1(s), W_2(s)$ and $W_3(s)$ – are the weighting functions depending on the frequency; S – is the sensitivity function; T – is the supplementary sensitivity function; R – is the control sensitivity function. The above functions are defined from the corresponding expressions [11]

Thus, the values of sensitivity functions must satisfy the following conditions

regulators is advisable to carry out in compliance with the following condition.

$$\left\{ \lim_{k \rightarrow \infty} \varepsilon_{\min}(x_i, k) = \lim_{k \rightarrow \infty} (\beta_i^*(x_i, \infty) - \beta(x, k)) = 0 \right\}_{i,k}, k \rightarrow \infty. \quad (9)$$

The simulation results of distributed control of ore

beneficiation technological line are presented in Fig. 2.

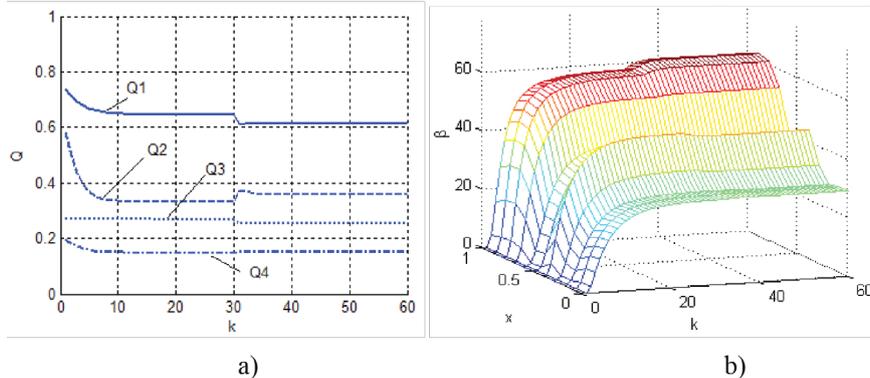


Figure 2. Dynamics of concentrated control signals and distributed output variable: a – beneficiation units control signals; b – distributed characteristics of the iron content in the ore

Thus, the considered control laws allow forming such control signals sequences for individual beneficiation units, which provide a minimum control error of the entire technological line under parametric uncertainty.

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