

# Method for research of parametric control schemes by asynchronous motor

**Vyacheslav Lobov**

*PhD, Associate professor of Computer Science,  
Automation and Control Systems department  
State Higher Educational Institution "Kryvyi Rih National University",  
Ukraine*

### Abstract

Asynchronous motor, in stator and rotor chains of which there used converters for control, is suggested. These convertors have resistors and thyristors, which are turned on between themselves in different ways, creating resistor- thyristor modules.

Scientific novelty is that while using these modules, generalized scheme of induction motor control is obtained. The scheme allows to get various models of parametric control, which may be used for investigation of different motor operating conditions on computer.

Key words: ASYNCHRONOUS MOTOR, THYRISTOR, RESISTOR, MODULE, GENERALIZED SCHEME

### **The problem and its connection with scientific and practical tasks**

The choice of power control circuit of asynchronous motor (AM) determines the possibility of electric motor of industrial plant on implementation of various modes. Technical and economic indicators of the power circuits play a primary role in the choice of the application area of asynchronous electric drives and show feasibility of their industrial application. Thought there is no exact thought where and in which case one should use this or that power schemes of parametric control of electric drive, and insufficiently substantiated choice of power scheme may lead to significant economic losses.

### **Analysis of research and publications**

Choice of rational scheme has the task of optimizing its quality. One solution to this problem is to analyze the existing domestic and

foreign practice different options schemes of thyristor power switches using experimental research. However as it was shown in [1-4] this way does not give an unambiguous answer to this task. Besides it may lead to wrong results, because using of this or that power scheme is determined by technical and economic terms regarding to mechanism [5-16].

### **Statement of the problem**

Comprehensive analysis of power management schemes and research of main modes of electric drive in order to choose from the electric power circuit switch and the technical requirements to Common mechanisms associated with the large volume of analytical calculations and experimental research. Therefore, for systematic analysis, finding or obtaining rational options of power schemes of asynchronous electric drive most convenient to use generalized (total) induction

motor control circuit and its mathematical description, which allows creating general algorithm for management and to use it effectively during research of electronic computer.

**Materials and results**

Modular way is suggested to build generalized scheme of control of AM. To implement this method basic modules should be used for building the scheme. Thus, the power module (PM) contains usually controlled valve and passive elements (resistors of active resistance R, capacitors C or inductance L). There are only passive elements in a communication module (CM). In PM instead of thyristor diodes triacs or other semiconductor devices can be used. Options R, C and L of elements that are in PM and CM are managed by impulsive, widely impulsive or other methods. Models become more complicated as parameters of the PM and CM should change with additional controlled devices and special management schemes.

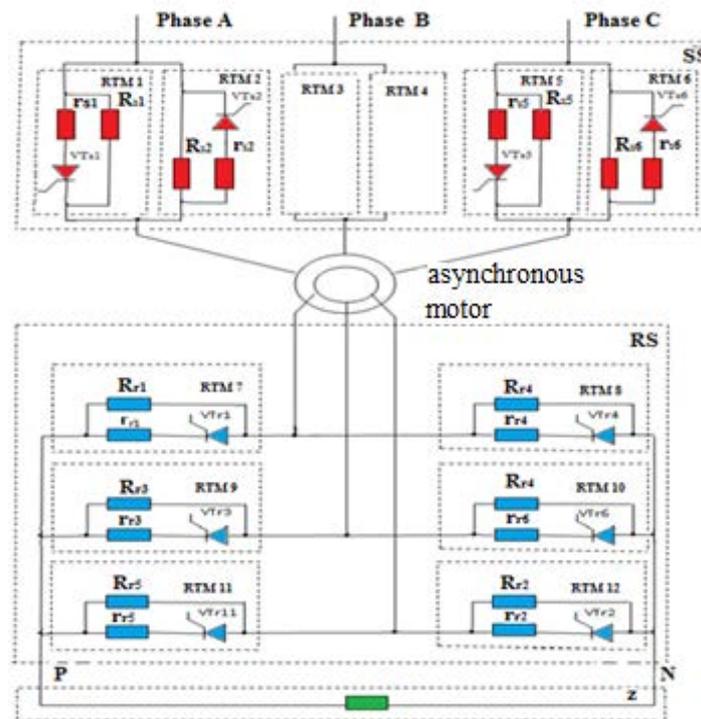
To get general structure for researching of electric drive work, such generalized control

scheme is necessary, which has enough quantity of simple modules to get maximum quantity of variants of power scheme of switches included in both stator and rotor induction motor circuit. Considering this, it is proposed to use a simple power module, where one part includes: two resistors, thyristor, and simple communication module, which contains only one active resistance resistor.

In schemes of converters for parametric control by stator and rotor chains of asynchronous electric drive various elements (devices with complete and incomplete handling) can be applied. Moreover, controlled elements are included both in the AC circuit and rectified current. They are included at output phase bridge rectifier.

Generalized scheme of parametric control of asynchronous motor with the help of these modules is obtained [12]. The power circuit is shown in the Fig.1.

Series connection of power thyristor and active resistor, where additional resistor is connected in parallel, forms a CM that is called resistor-thyristor (RTM).



**Figure 1.** Generalized scheme of AM parametric control

Each RTM is not only individual functional element, but also constructive complete unit (module). Generalized scheme of parametric control of asynchronous motor

includes stator irreversible (SS) and rotary (RS) switches formed with RTM. In each phase induction motor includes a stator-to-parallel connected RTM and spinning - consists of six

RTM included on the bridge circuit. Between P and N points rotary switch (Fig. 1) communication module of Z type is connected, which forms the DC link.

Communication module of Z type has three different devices:  $Z_0, Z_s, Z_i$  forming the groups of RS. The first group  $Z_0$  is created by devices that short circuit. The second group  $Z_s$  has devices that let discretely change the parameter elements included in the communication module Z. Third group  $Z_i$  has devices that fulfill pulse adjusting of these parameters. In the generalized scheme of parametric control by asynchronous motor there used communication module of Z type, which provides change in law the value of active resistor included between P and N points. CM are made of two types, which has non-contact switching device or thyristor AC voltage. Contactless switching devices have only two states (on and off) and that is why are called uncontrolled or unregulated.

Controlled or adjustable SM consisting of thyristors (triacs) are supplemented by electronic protection equipment, entrance control circuits, impulse makers to control the thyristors, there is also systems of pulse-phase control (SPPC) and computer aided starting and stopping of electric drive systems necessary for control implementing of induction motor.

Generalized scheme of parametric control of asynchronous motor provides a power scheme both common and separate management of stator and rotor circuits. Under the joint control we mean control with the help of SS and RS simultaneously in the stator and rotor, and under separate - only using the SS in the stator or just using the RS in the rotor asynchronous motor. Let us consider the possibility of the proposed generalized scheme of asynchronous motor with active resistor in the stator chain, indicated in RTM1- RTM6 as:  $R_{si} i r_{si}$  and RTM7-RTM12 rotor as  $R_{ri} i r_{ri}$ , provided that:

$R_{si} = R_s; R_{ri} = R_r; r_{si} = r_s; r_{ri} = r_r$ , where  $i = 1, 2, \dots$  for the boundary (0,  $\infty$ ) and intermediate values of variables  $R_s, r_s, R_r$  and  $r_r$  and three devices  $Z_0, Z_s, Z_i$ , connection module Z. In accordance with accepted restrictions in Table. 1 and 2 there shown the possible circuits respectively for the SS and RS, which are marked by:  $S_{ij} i Z_{kij}$ . Indices ij indicate the serial number of the relevant row and column in the table, and index K is set to 0, s, i, that is, it indicates the type of communication module Z.

AM control schemes containing SS and RS types:

$S_{11}, S_{21}, S_{31}$ , and  $Z_0R_{11}, Z_0R_{21}, Z_0R_{31}, Z_sR_{11}, Z_sR_{21}, Z_sR_{31}$

$Z_iR_{11}, Z_iR_{21}, Z_iR_{31}$ , are separate control schemes in the stator and rotor. Despite restrictions, proposed generalized scheme covers many well-known circuits of parametric control of asynchronous motor, as it is illustrated by the following examples.

So the analysis and description of separate parametric control circuit using thyristors in stator type  $S_{j3}$  are shown in [9, 14, 15].

**Table 1.** Variants of SS

$r_{si}$	$R_{si}$		
	0	const	$\infty$
0	$S_{11}$	$S_{12}$	$S_{13}$
const	$S_{21}$	$S_{22}$	$S_{23}$
$\infty$	$S_{31}$	$S_{32}$	$S_{33}$

**Table 2.** Variants of RS

$Z_k$		$R_{ri}$		
		0	const	$\infty$
$Z_0$	const	$Z_0R_{11}$	$Z_0R_{12}$	$Z_0R_{13}$
	$\infty$	$Z_0R_{21}$	$Z_0R_{22}$	$Z_0R_{23}$
	0	$Z_0R_{31}$	$Z_0R_{32}$	$Z_0R_{33}$
$Z_s$	const	$Z_sR_{11}$	$Z_sR_{12}$	$Z_sR_{13}$
	$\infty$	$Z_sR_{21}$	$Z_sR_{22}$	$Z_sR_{23}$
	0	$Z_sR_{31}$	$Z_sR_{32}$	$Z_sR_{33}$
$Z_i$	const	$Z_iR_{11}$	$Z_iR_{12}$	$Z_iR_{13}$
	$\infty$	$Z_iR_{21}$	$Z_iR_{22}$	$Z_iR_{23}$
	0	$Z_{31}R_{11}$	$Z_iR_{32}$	$Z_iR_{33}$

In [4, 6] as RS there used scheme of  $Z_iR_{11} t$  type. Schemes  $Z_0R_{13}$  and two parallel circuits  $Z_iR_{13}$  are given in [6-11]. Operation of separate parametric control circuits in the rotor of  $Z_0R_{12}, Z_0R_{33}, Z_sR_{13}$  types is considered in [1, 4, 5] and  $Z_iR_{13}$  - in [11-14]. The analysis and experimental research of scheme  $Z_sR_{13}$  for Z, including  $R_r i r_r = const$ , are given in [9], and parametric control circuit of common types  $S_{13}Z_sR_{ij} i S_{13}Z_iR_{ij}$ - [12, 14] and the type  $S_{13}Z_0R_{32}$  - [1, 2, 9-11].

Numerous application options of SS for obtaining not only rotating but still fields AM and other modes are considered in [1-16].

Generalized scheme for irreversible SS allows to obtain nine options for various types of power circuits. Two schemes  $S_{12}$  and  $S_{13}$  that are shown in Fig. 2 are of great interest for comparative analysis. Scheme of  $S_{12}$  type (Figure 2, a) is provided for the case when  $R_{si} = const$  and  $r_{si} = 0$ , and the structure of the

circuit of  $S_{13}$  type (Figure 2, b), for  $R_{si} = \infty$  и  $r_{si} = 0$ . Stator winding of asynchronous motor in circuit of  $S_{12}$  type is connected to the mains via RTM, and the circuit of  $S_{13}$  type, - via thyristor module (TM). The circuit of  $S_{12}$  type RTM includes a resistor of resistance  $R_{si}$ , which is parallel to connected thyristor  $VT_i$ . Moreover, each phase of induction motor stator includes two RTM, interconnected-to-parallel.

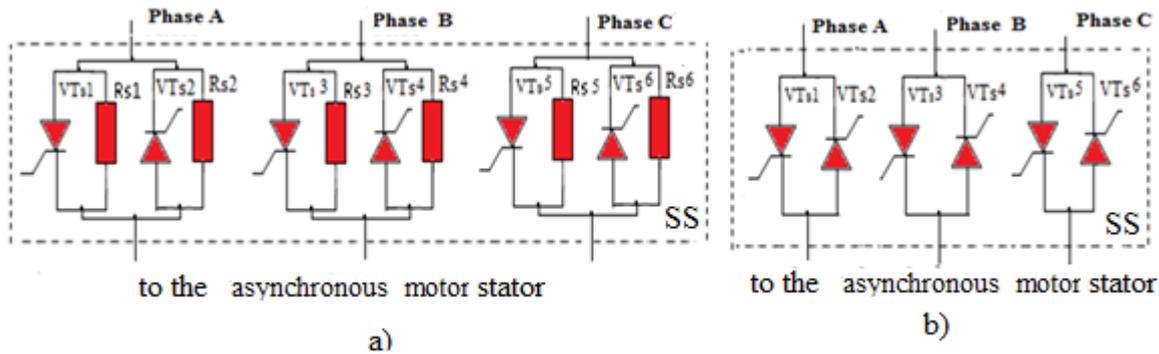


Figure 2. SS Power schemes of  $S_{12}$  (a) i  $S_{13}$  (b) types

Scheme of  $S_{13}$  type consists of thyristors and resistors  $R_{si}$  and  $r_{si}$  in this module are not available. In each phase of AM stator AM, there included two thyristors, which are interconnected-to-parallel circuit, and form irreversible known thyristor voltage regulator (TVR) [14, 15]. Please note that the converters that have some kind of valve elements with incomplete handling (thyristor or triac) are included in AC circuits, work in natural mode switching. This converter type implements the so-called phase control in stator or rotor, as it will be shown below, the asynchronous motor circuits [14, 15].

There are twenty-seven different power control schemes of rotor chain of asynchronous motor in the Table 2. Options for power control schemes of AM rotor circuit:

$$Z_0R_{11}, Z_0R_{21}, Z_0R_{31}, Z_sR_{11}, Z_sR_{21}, Z_sR_{31}, Z_iR_{11}, Z_iR_{21}, Z_iR_{31}$$

$R_{ri} = 0$  provides only locking of circuit rotor winding to the common connection point, thus turning the rotor in short-usual one.

Let us consider the power circuit of RS, which have included RTM in rotor circuits, with the help of which starting and brief regulation of AM rotor speed is provided. Under the scheme of generalized parametric control of asynchronous motor (Fig. 1) at  $R_{ri} =$

$const$  and  $r_{ri} = const$  in each phase induction motor rotor parallel to resistance  $R_{ri}$  there included series-connected circuit between a resistor  $r_{ri}$  and thyristor  $VT_{i-}$  when  $R_{ri} = \infty$  and  $r_{ri} = const$  there is only connected in series circuit with these items. All this leads to different power circuits. Thus, when  $R_{ri} = const$  there formed different types of schemes  $Z_kR_{12}, Z_kR_{22}$  i  $Z_kR_{32}$ , while  $R_{ri} = Z_kR_{13}, Z_kR_{23}, Z_kR_{33}$  and a number of other schemes listed in the table. 2. Scheme of  $Z_kR_{13}$  type (Fig. 2.3, a) when  $r_{ri} = 0$  is known as Larionov bridge circuit [16, 17], where communication module of  $Z_k$  type is suggested in the constant current circuit. Two other schemes such as  $Z_kR_{22}$  (at  $R_{ri} = const, r_{ri} = const$  and  $Z_k = \infty$ ) and  $Z_kR_{23}$  with  $R_{ri} = \infty$  and  $r_{ri} = const$  and  $Z_k = \infty$ ) don't have DC open circuit, and can be used independently.

Using the communication module of  $Z$  type, appropriate  $Z_0$  the schemes of  $Z_kR_{22}$  type will be converted into a type scheme  $Z_0R_{32}$ , and scheme of  $Z_kR_{23}$  type in accordance with  $Z_0R_{33}$  type. In addition, from scheme of  $Z_0R_{32}$  type at  $R_{ri} = \infty$  and  $r_{ri} = const$  there is a new type of scheme  $Z_0R_{13}$ , while  $R_{ri} = const$  and  $r_{ri} = \infty$ , scheme of  $Z_0R_{22}$  type is widely used in industrial environments. It contains only additional

resistors in the rotor circuit. When  $R_{ri}=const$  and  $r_{ri}=0$  the output of  $Z_0R_{32}$  type (Figure 3, c) and at  $R_{ri}=const, r_{ri}=0$  - type  $Z_0r_{33}$  (Fig. 3, d). Similarly, from the scheme of  $Z_0R_{33}$  type at  $r_{ri}=0$  there created another scheme of  $Z_0r_{33}$  type, where the rotor windings are connected in "stars" circuit and consistently connected to the thyristors and resistors locked together in the zero point. The above-mentioned power circuits

are shown in the Fig. 4. The power structure will change significantly for the scheme of  $Z_0R_{32}$  type, if in circuit DC circuit there will be devices of  $Z_s$  or  $Z_i$  type. From the scheme of  $Z_{s(i)}R_{32}$  type there obtained rotary switch, which thyristors are connected in triangle.

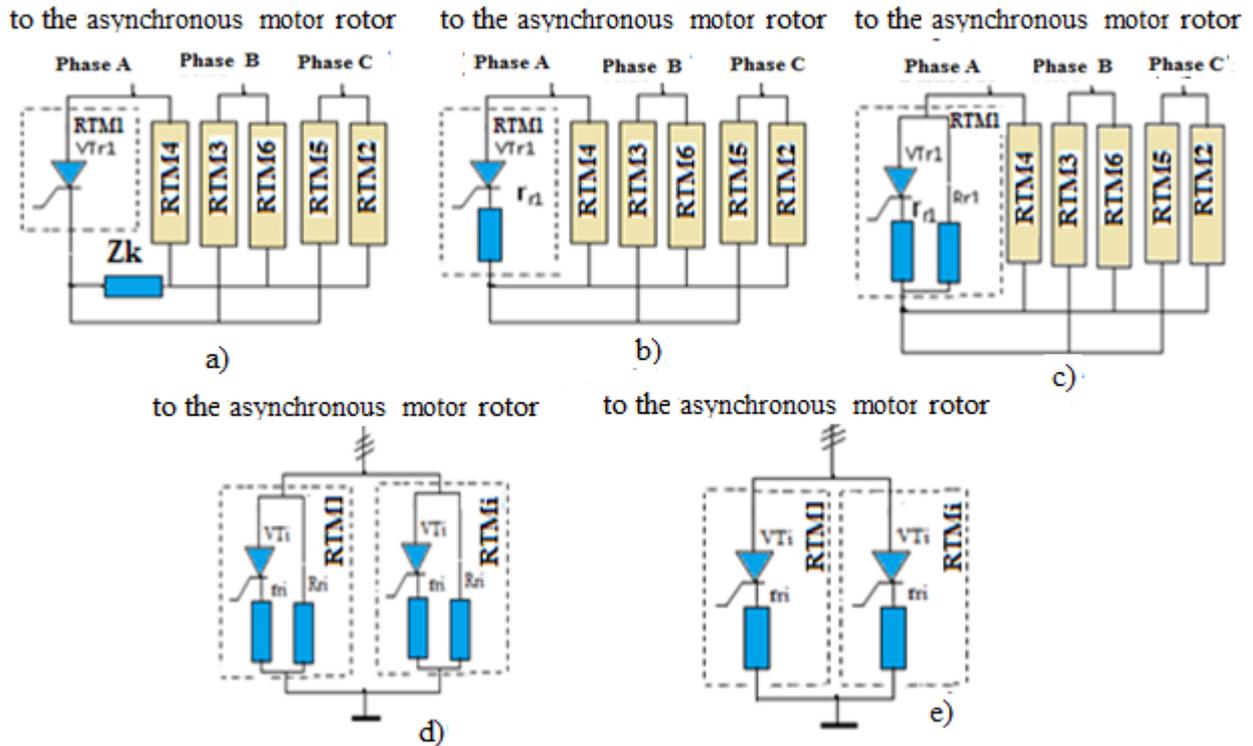


Figure 3. Power schemes of RS types  $Z_kR_{13}$  (a),  $Z_kR_{23}$  (b),  $Z_kR_{22}$  (c),  $Z_0R_{32}$  (d) i  $Z_0R_{33}$  (e)

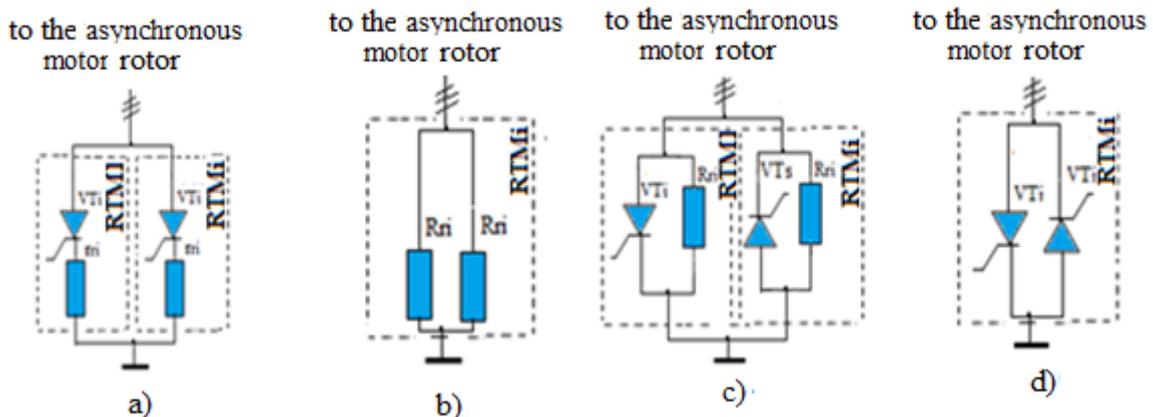


Figure 4. Power schemes of RS types  $Z_kR_{32}$  with connection modules  $Z_0(i)$ :  $Z_0r_{13}$  (a),  $Z_0r_{22}$  (b),  $Z_0r_{23}$  (c) i  $Z_0r_{33}$  (d)

In this case, device  $Z_s$  or  $Z_i$  is only one thyristor included into direct current circuit. If we accept that the generalized scheme of  $Z_{s(i)}R_{32}$  type (Figure 5, a) resistor:  $R_{r1} = R_{r2} = R_{r3} = R_{r4} = R_{r5} = R_{r6} = \infty, r_{r2} =$

$r_{r3} = r_{r5} = r_{r6} = \infty = r_{r2} = const, r_{r1} = r_{r4} = 0$ , we find that the triangular switch is included in the zero point connection of rotor of induction motor and there is power circuit of  $Z_1R_{32}$  type (Fig. 5, b).

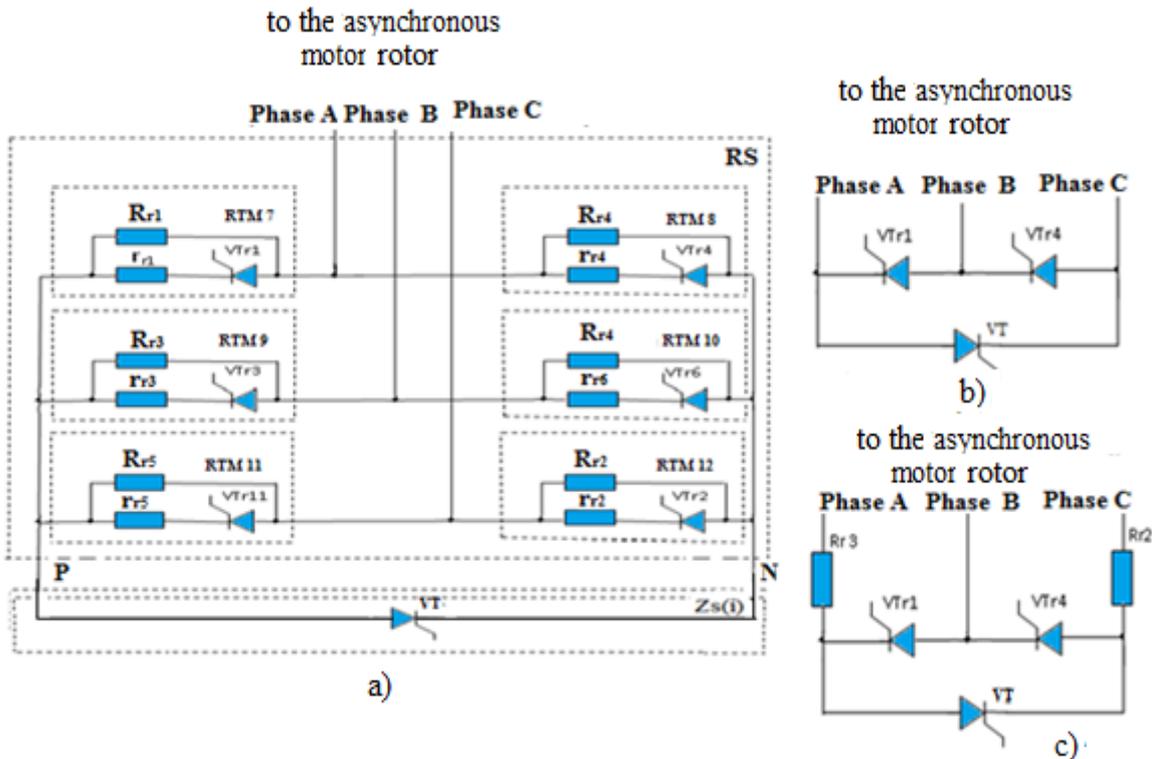


Figure 5. Power schemes of RS types:  $Z_{s(i)}R_{32}$  (a),  $Z_1R_{32}$  (b) i  $Z_2R_{32}$  (c)

As it is seen from the scheme provided in Fig. 5, there is no resistor in the rotor circuit. If we take in circuit of  $Z_{s(i)}R_{32}$  type, that  $R_{r1} = R_{r4} = R_{r5} = R_{r6} = \infty = const$ , and  $r_{r1} = r_{r4} = 0$   $r_{r2} = r_{r3} = r_{r5} = r_{r6} = \infty = r_{r2} = const$ , then the switch will be turned on according to the scheme  $Z_2R_{32}$  (Figure 5, c). In the obtained scheme only in phases B and C resistors  $R_{r3}$  and  $R_{r6}$  are included, but in phase A they are missing. For getting resistor of all three phases of rotor induction motor, it is necessary to add generalized scheme with a new RTM and to change the structure of connection module of Z type.

The above-mentioned schemes have practical application in many common industrial electric drives of mechanisms, including conveyor installation, drawing, wire, tube-drawing bench [5-15]. If you select the power scheme from generalized scheme, there should be considered that the thyristors RTM, included into the SS and RS work with the same angles of ( $\alpha$ ) opening. If for one group of thyristors, for example, in the scheme of  $S_{13}$  type one takes angles of opening of SC  $\alpha_s = 0 \wedge 0$  (open state), the thyristor modules are converted into equivalent thyristor - diode modules (TDM).

Similarly, if in the circuit RS to assume that one group of thyristors  $VTr_2, VTr_4$  and  $VTr_6$  will be fully open (opening angle of thyristors  $\alpha_r = 0^\circ$ ), then the rotor circuit there will be turned on consisting of the equivalent TDM.

This property of generalized scheme of asynchronous motor can be used for the selection, analysis and study of power switching circuits using ECM. All the power schemes of asynchronous motor with SS and RS derived from generalized parametric control schemes can be divided into two main groups: with phase and impulse control switches. In the first group the control is fulfilled due to the natural switching valves RTM. Schemes of phase control valves for conventional circuit rotor are more complicated than general ones, applied for stator asynchronous motor circuits. The main distinguishing feature of them is in terms of synchronization blocks operation that should consistently run the application in a wide range frequency and amplitude of the rotary voltage.

### Conclusions

Thus, using the most simple resistor-thyristor modules and elementary communication modules made it possible to obtain a generalized scheme of induction motor control. This scheme brought together a variety

of known schemes and schemes of parametric control previously not considered. The structure of the scheme can be used in the analysis and study of starting, braking, energy and other operating modes of series of power circuits of asynchronous electric drives control. Changing parameters of RTM resistor and communication modules in the structure of generalized scheme of induction motor, it is possible to obtain almost any version of power scheme for electric motor control necessary for research or manufacturing application.

### References

1. Petrushin V. S, Yakymets A. M, Ermolaev V. V. (2012). Comparative analysis of different launching modes of short-circuited asynchronous engine // *Electromechanical and saving system*. No 3, p.p. 243-246.
1. 2. Figaro B. I. (2011). Applying devices of smooth start and inhibition of asynchronous electric motors with a short-circuited rotor in electric drive of crane mechanisms of movement. *Electrotechnical and computer systems*. No 4, p.p. 30-38
2. Patent UA №101843. Control method of tiristor voltage regulator in device of deceleration start of asynchronous motor. Marenych K. M, Russiyan S. A IPC (2013.01), H02M 7/00 H02M 1/08 (2006.01), H02J 3/18 (2006.01), H02P 7/00, H02P 5/00, H02M 5/00, 13.05.2013, Bull. Number 9
3. Krasnoshapka N. D. (2011). Reducing the error calculation of starting modes of asynchronous electric drives for static characteristics. *Problems of information and management: Coll. Science. works*. Kiev, NAU, No 3 (35), p.p. 62-67.
4. Vasilyev D. S. (2010). Research of electromechanical processes with direct start and inhibition of asynchronous engines with records of variable parameters and its comparison with smooth starting and inhibition. *Bulletin of Kremenchug state-owned university named after Mikhail Ostrohradskii*. No 4, p.p. 43-49.
5. Patent UA № 67058. Method of forming starting modes asynchronous drive with phase rotor. Kovalev V. I. IPC (2011.01) E21B 4/00, E21B 44/00, 25.01.2012, Byul.№ 2, 2012
6. Marenych K. M., Russiyan S. A. (2010). Justification principle of improving the method of deceleration start asynchronous electric mining machine. *Mining electrician and automatics*. Vol. 84, p.p. 160-168.
7. Kalinov A. P. Yukhimenko M. U, Isaev S. V. (2007). Research of the effectiveness launcher the formative regimes of asynchronous engine. *Electrical and energy saving systems*. No 2 (2), p.p.15-21.
8. Chernyi A. P, Hladyr A. I, Osadchyk U. G. Launcher system of unregulated electric drives. Monograph. Kremenchug, "Scherbatyh A.V." Private Company. 2006, 280 p.
9. Popovich M. G, Lozinsky O. U., Klepikov V. B. Electromechanical automatic control system and electric drives: manual. guide. Kiev, Lybid, 2005, 680 p.
10. Zyuzev A. M., Kostilev A. V., Stepaniuc D. P. Method of smooth start asynchronous engine with short circuit rotor. RF Patent number 2497267, IPC H02P1 / 26, H02P1 / 28, 10.27.2013, Bull. Number 30.
11. Lobov V. I. Research of launcher and braking regimes of asynchronous electric drive with teristor parametric control. Abstract of thesis for the degree of PhD. tehn. Sciences. Moscow. VNYY electric drive, 1983.
12. Davydenko A. G, Lobov V. Y. Paryshkura N. G, Ruhlenko S. K, Petrov P. E. Electric drive of variable current. A. p. USSR No 944034, class H 02 P 3/24, H 02 R 5/28 from 07/18/82 h.- 4 p.
13. Chylykyn M. G. Sandler A. S. General course of electric drive. Textbook for Universities. Moscow, Energoizdat, 2007, 576 p.
14. Thyristor voltage converters for asynchronous electric / L.P. Petrov, O. A. Andryushchenko, V. I. Kapynos. Moscow, Energoatomizdat, 1986, 200 p.
15. Liudmyla Yefimenko, Mykhailo Tykhanskyi (2015). Dynamic load reduction techniques for the flight of the belt. *Metallurgical and Mining Industry*, No2, p.p. 47-51.